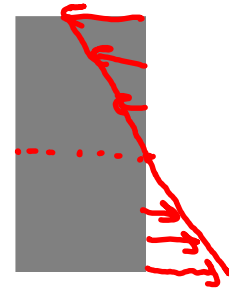
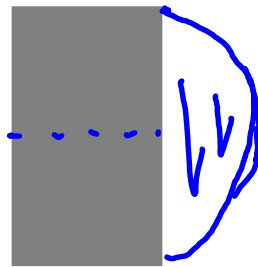


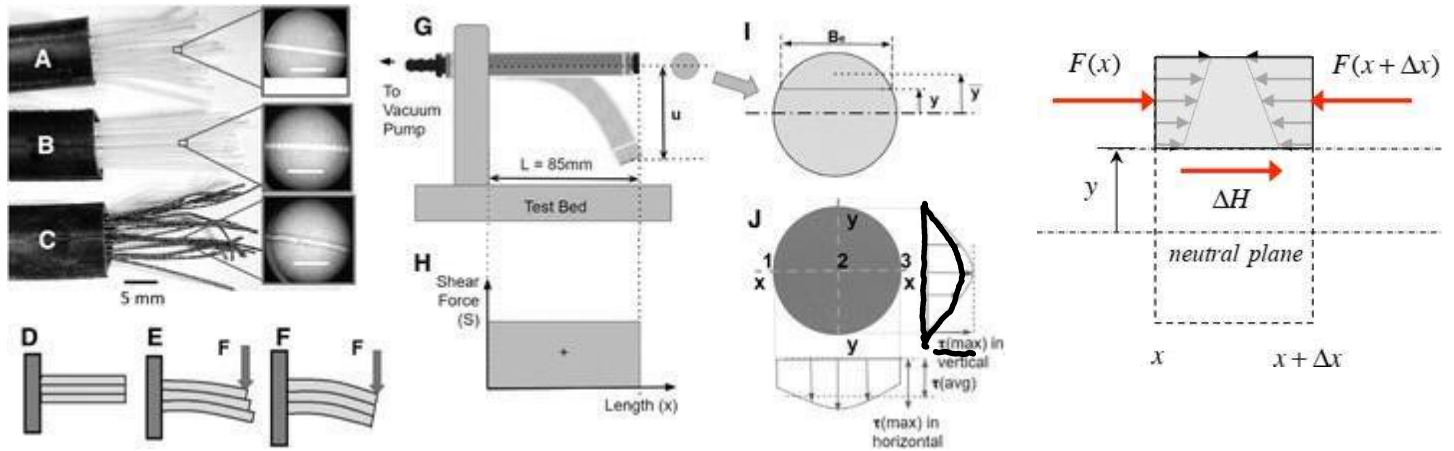
# Lecture 14 Review

For a rectangular cross-section: at the neutral plane, the shear stress is \_\_\_\_\_ and the normal stress is \_\_\_\_\_.

- zero, zero
- zero, maximum
- maximum, zero
- maximum, maximum

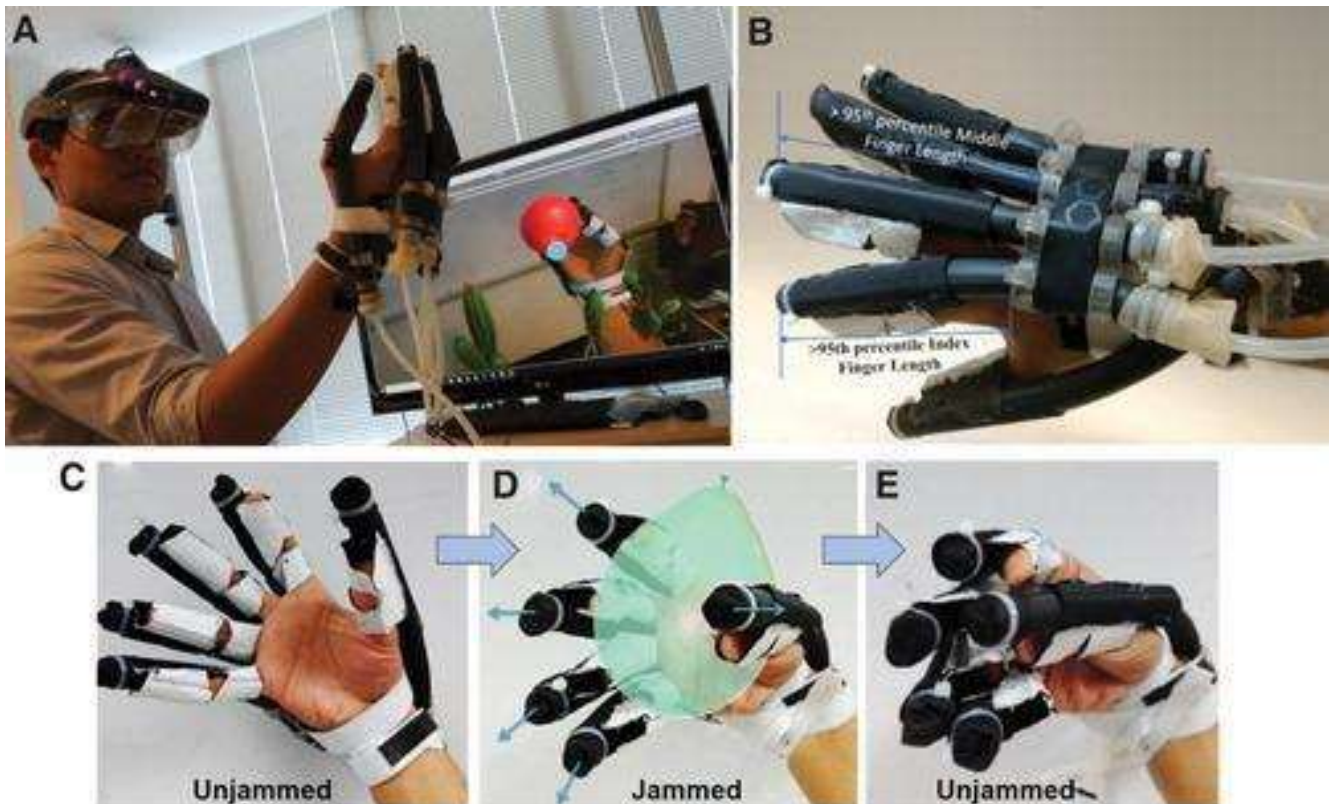


# Shear and Normal Stresses in Practical Robots



$$\tau_{induced} = k_{correction} \times \frac{SA_e \hat{y}_e}{I_e B_e}, \quad (1) \quad \frac{VA_e}{It}$$

where  $A_e$  is the area of the cross section beyond the section at a distance of  $y$  away from the neutral axis,  $\hat{y}_e$  is the centroid of that area away from the neutral axis, and  $B_e$  is the width of the section at a distance of  $y$  from the neutral axis. The accuracy of the above shear stress formula depends on the aspect ratio of the cross section of the ellipse. For very high

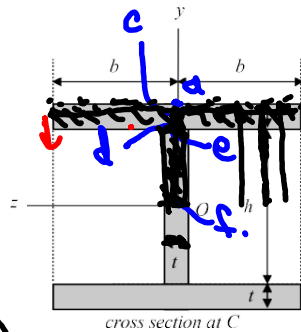


$$\tau = \frac{VA\bar{y}_a}{It}$$

**Example 10.5**

The cantilevered beam shown below is loaded in pure bending. The beam has a cross section at location C on the beam as shown below right. The origin O is located on the neutral axis of the beam.

- a) Determine the second area moment  $I_{Oz}$  corresponding to the neutral axis of the beam.
- b) Determine the distribution of normal stress on the cross section of the beam as a function of  $y$ .
- c) Determine the maximum (magnitude) normal stress occurring on the cross-sectional face at C.



$b = 80 \text{ mm}$   
 $t = 20 \text{ mm}$   
 $h = 100 \text{ mm}$   
 $I = 2.492 \times 10^{-5} \text{ m}^4$

d) Find shear stress distribution on cross-section.

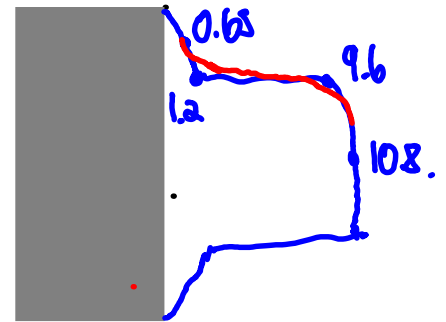
$$\tau_a = \frac{VA\bar{y}_a}{It} = 0$$

$$\tau_c = \frac{V\left(\frac{t}{2}\right)(2b)\left(\frac{h}{2} + \frac{3}{4}t\right)}{I(2b)} = 0.65 \times 10^{-3} \left(\frac{V}{I}\right)$$

$$\tau_d = \frac{V(t)(2b)\left(\frac{h}{2} + \frac{1}{2}t\right)}{I(2b)} = 1.2 \times 10^{-3} \left(\frac{V}{I}\right)$$

$$\tau_e = \frac{V(t)(2b)\left(\frac{h}{2} + \frac{1}{2}t\right)}{I(t)} = 9.6 \times 10^{-3} \left(\frac{V}{I}\right)$$

$$\tau_f = \frac{V\left[2bt + \frac{h}{2}t\right]\bar{y}_f^*}{It} = 10.8 \times 10^{-3} \left(\frac{V}{I}\right)$$



$$\bar{y}_f^* = \frac{\bar{y}_1 A_1 + \bar{y}_2 A_2}{A_1 + A_2}$$

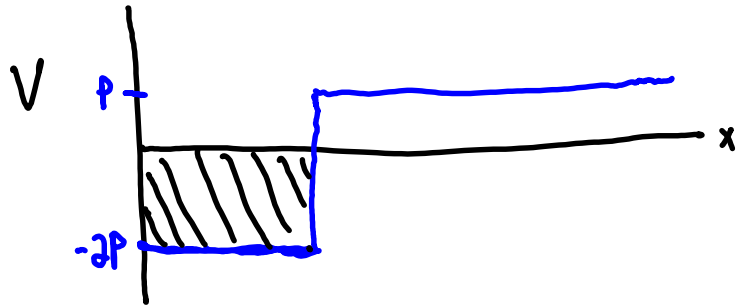
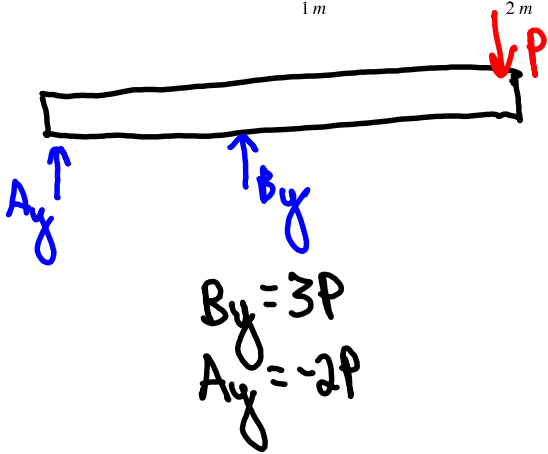
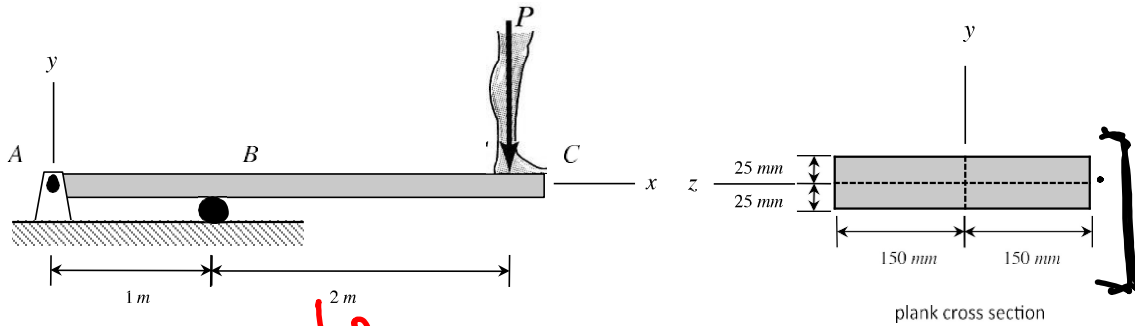
$$\bar{y}_f^* = \frac{\left(\frac{h}{4}\right)\left(\frac{h}{2}t\right) + \left(\frac{h}{2} + \frac{t}{2}\right)(2bt)}{\left(\frac{h}{2}t\right) + (2bt)}$$

$$\bar{y} = \frac{1}{A} \int y dA$$



### Example 10.10

A timber plank is to be used as a diving board. The diving board is held down at end A by a steel strap that is secured by anchor bolts and rests on a roller at location B. Calculate the maximum permissible load  $P_{max}$  such that the maximum normal stress in the diving board does not exceed  $11 \text{ MPa}$ .



$$\sigma_{max} = \frac{-M_y}{I_y} = \frac{(2P)(\frac{L}{2})}{\left(\frac{bh^3}{12}\right)} = \frac{12P}{bh^2}$$

$$P = \frac{bh^2}{12} |\sigma_{max}|$$

$$P_{max} = \frac{(0.3\text{m})(0.05\text{m})^2}{12} (11 \times 10^6 \text{ Pa})$$

$$P_{max} = 687 \text{ N} = 70 \text{ kg} = 154 \text{ lbs.}$$

